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# The effect of frequency on the velocity and attenuation of the bulk metallic glass $Zr_{41.2}Ti_{13.8}Cu_{12.5}Ni_{10.0}Be_{22.5}$ under high pressure

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### Abstract

Using the pulse echo overlap method and the pulse superposition method, the acoustic velocities  $V_l$ ,  $V_s$  and the attenuations  $\alpha_l$ ,  $\alpha_s$  of Zr<sub>41.2</sub>Ti<sub>13.8</sub>Cu<sub>12.5</sub>Ni<sub>10.0</sub>Be<sub>22.5</sub> bulk metallic glass have been measured below 2 GPa with 10 and 20 MHz carrier frequencies, respectively. The results reveal that  $V_l$  and  $V_s$  increase linearly with increasing pressure (*P*); the slope of the  $V_l-P$  curve decreases with increasing frequency, while that of the  $V_s-P$  curve increases with increasing frequency. This means that there is a slight dispersion of sound under pressure. The attenuation increases obviously with the carrier frequency from 10 to 20 MHz. The effects of frequency on the velocity and attenuation under high pressure are discussed.

## 1. Introduction

 $Zr_{41.2}Ti_{13.8}Cu_{12.5}Ni_{10.0}Be_{22.5}$  bulk metallic glass (Zr/Ti BMG) prepared by the melt-quenching technique is a new multicomponent amorphous alloy material. This amorphous alloy has generated great interest in recent years, because it exhibits many unique physical properties and has potential for applications [1]. However, some of the properties are still ambiguous, so it is important to establish the inherent relations between the physical properties and microstructure for this amorphous alloy.

Acoustic velocity and attenuation are two very useful parameters in ultrasonic studies. The velocity of an acoustic wave propagating through an elastic medium is related closely to the structure and state of the medium itself. It can be represented by a function of the density and elastic constants. Acoustic attenuation characterizes the energy loss caused by viscosity, anelasticity, relaxation, etc, when an acoustic wave propagates through a medium. Measuring the velocity and attenuation of BMG under high pressure and at different frequencies can

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Figure 1. The relative changes of  $V_l$  and  $V_s$  measured under high pressure using the PEO and PSP techniques, respectively.

provide many significant experimental data relating to elastic behaviour, plastic deformation, the equation of state, etc, and can also provide some important information about the behaviour when its general structure and microstructure are changed.

### 2. Experiment

The pulse echo overlap (PEO) [2] and pulse superposition (PSP) [3] methods are two different techniques based on ultrasonic interferometry. They are used to measure the time taken to travel through the sample; the measured quantity is the frequency, which is measured with a precision better than  $10^{-5}$ .

Usually, the acoustic attenuation coefficient  $\alpha$  is defined [4] by

$$\alpha$$
 (dB cm<sup>-1</sup>) = (20/2L) log<sub>10</sub>( $E_n/E_{n+1}$ )

where L is the length of the sample, and  $E_n$  and  $E_{n+1}$  represent the amplitudes of two arbitrary neighbouring echoes in the pulse echo series.

 $V_l$  and  $\alpha_l$  for longitudinal waves were measured simultaneously by a MATEC ultrasonic measuring system.  $V_s$  and  $\alpha_s$  for shear waves were measured in a similar manner.

High-pressure experiments were completed in a two-piston–cylinder high-pressure apparatus using the PEO and PSP techniques. The pressure was calibrated using a manganin resistance gauge. In the PEO study, pressure was exerted up to 0.5 GPa, the carrier frequency was 10 MHz, and the pressure medium was a 1:1 liquid mixture of transformer oil and kerosene. In the PSP study, pressure was exerted up to 2 GPa, the carrier frequency was 20 MHz, and the pressure medium was a 1:1 liquid mixture of pentane. Here it is worth noting that changes of the length and density for the sample under the high pressure of 2 GPa have to be considered. We made corrections to the length and elastic modulus from the experimental data using the Cook method [5].

The relative changes of  $V_l$  and  $V_s$  measured by the PEO and PSP techniques under high pressure are shown in figure 1. Those of  $\alpha_l$ ,  $\alpha_s$  are shown in figure 2.

Incidentally, the data measured using the PEO and the PSP techniques for a given sample are in conformity [6], and have the same measuring precision.



**Figure 2.** The curves for  $\alpha_l$  and  $\alpha_s$  versus pressure obtained using the PEO and PSP techniques, respectively.

# 3. Results and discussion

Figure 1 reveals that both  $V_l$  and  $V_s$  increase linearly with pressure up to 2 GPa, because Zr/Ti BMG exhibits the properties of a homogeneous elastic solid in the compressed state. The slopes of the  $V_l-P$  and  $V_s-P$  curves at 10 MHz are  $5.97 \times 10^{-2}$  and  $1.1 \times 10^{-2}$  km s<sup>-1</sup> GPa<sup>-1</sup>, respectively. The slopes of the  $V_l-P$  and  $V_s-P$  curves at 20 MHz are  $5.52 \times 10^{-2}$  and  $1.39 \times 10^{-2}$  km s<sup>-1</sup> GPa<sup>-1</sup>, respectively. By comparison, in the pressure range below 0.5 GPa, the slope of the  $V_l-P$  curve decreases slightly when the carrier frequency is raised from 10 to 20 MHz, but that of the  $V_s-P$  curve increases. This means that there is a slight dispersion of sound under high pressure for Zr/Ti BMG.

Similarly, figure 2 reveals that  $\alpha_l$  and  $\alpha_s$  increase monotonically with pressure up to 2 GPa. The changes for the longitudinal modes ( $V_l$  and  $\alpha_l$ ) are much larger than those of the shear modes ( $V_s$  and  $\alpha_s$ ) at both 10 and 20 MHz, and  $\alpha_l$ ,  $\alpha_s$  increase with the frequency. This is because the propagation of an ultrasonic wave is basically an adiabatic process. When a compressive wave passes through the sample, the heat flow between the compressed and expanded parts in it leads to energy loss. This loss is related to the frequency [7] and the longitudinal velocity. In contrast, at lower frequency (10 MHz), the  $\alpha_s$ –*P* curve shows a fluctuation below 0.5 GPa: there is a maximum near 0.15 GPa and a minimum near 0.35 GPa.

The random arrays of atoms of the metallic glass and the local anomalous areas in the random arrays can affect the elasticity and anelasticity. The fluctuations of the local structure and density under pressure can lead to fluctuation of the local stress on the atomic scale. The local tensile stress areas can achieve viscous flow easily under pressure; a 'liquid-like-state' viscosity is exhibited. But the local compressive stress areas have more difficulty in flowing; a 'solid-like-state' rigidity is exhibited.

The bulk modulus *B* and its pressure derivative B' can be obtained from the measured pressure dependences of  $V_l$  and  $V_s$  under 2 GPa.  $B_0$  and  $B'_0$  determined for Zr/Ti BMG are 114.75 GPa and 4.059, respectively. So the isothermal Murnaghan equation of state can be written as follows:

$$P = (B_0/B'_0)[(V_0/V)^{B'_0} - 1] = 28.27[(V_0/V)^{4.059} - 1].$$

Here V is the volume.

# 4. Conclusions

In the short range, correlating closely with atomic configurations, non-metallic glasses such as oxide glasses form chain-like or network structures; the bond angles between atoms change under pressure, and this leads to negative pressure dependence. All BMGs have densely randomly packed microstructures with metallic bonds. The velocity and attenuation are related to the microstructural configuration and the glass-forming ability [8]. For Zr–Ti BMG the pressure dependence exhibits different characteristics as compared with that for oxide glasses. The experimental results show that both  $V_l$  and  $V_s$  increase with pressure and the slopes of the  $V_l-P$  and  $V_s-P$  curves change with the carrier frequency. These findings indicate a stiff modulus and a slight dispersion of sound under hydrostatic pressure. The attenuation increases obviously with carrier frequency from 10 to 20 MHz. The  $\alpha_s-P$  curve shows a fluctuation.

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